

## Preparation of Ceria-zirconia Mixed Oxides with Improved Thermal Stability for Three-way Catalysts by a Modified Co-precipitation Method

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**Abstract:** A series of ceria-zirconia mixed oxides (CZ- $x$ ;  $x=0, 20, 40$  and  $80$ ) with Ce/Zr molar ratio of  $3/2$  were synthesized by co-precipitation method. In order to improve the thermal stability of ceria-zirconia mixed oxides, we extended the time for the primary grain to grow up by a modified synthesis reactor. The resulting samples were characterized by X-ray diffraction (XRD),  $N_2$  adsorption-desorption, and transmission electron microscopy (TEM). The results revealed that bigger grain could be obtained by extending time for the primary grain to grow up, which was propitious to enhance the textural properties and structural properties of the materials. Thus, the thermal stability of the materials was improved. In this study, the materials were applied in the field of Pd-only three way catalysts (TWCs). The catalysts exhibited excellent catalytic performance and thermostability, showing better prospect in application.

**Key words:** ceria-zirconia composites; primary grain; co-precipitation; thermostability

The emissions of pollutants from automotive exhausts have caused the air pollution around our living cities<sup>[1-2]</sup>. Currently, the most effective way for the gasoline engine cars is the equipment of three-way catalytic converters which can convert the primary pollutants of carbon monoxide (CO), hydrocarbons (HCs) and nitrogen oxides ( $NO_x$ ) into relatively environmentally friendly products of  $CO_2$ ,  $H_2O$  and  $N_2$  under actual conditions<sup>[3-5]</sup>. Ceria-zirconia mixed oxides have been widely applied for automotive three-way catalysts (TWCs) because of stronger redox and oxygen storage abilities<sup>[6]</sup>. However, higher exhaust temperatures ( $>1000^\circ C$ ) must demand a better thermal stability of TWCs in applications<sup>[1, 7]</sup>.

Many efforts have been spent to improve the thermal stability of ceria-zirconia mixed oxides<sup>[8-11]</sup>. It has been found that many factors could affect the thermal stability of the oxides<sup>[3, 8, 12]</sup>, wherein the pore structure of materials is the main one<sup>[7]</sup>. Broadly speaking, larger pores could prevent the sintering of the materials. And larger pores are usually piled up by larger crystalline grains. Therefore, the aim of this study is to improve thermal stability of ceria-zirconia mixed oxides by a modified co-precipitation method, which can increase the crystalline size of materials.

## 1 Experimental

### 1.1 The modified co-precipitation method

A modified co-precipitation method was designed (Fig. 1) and used for the synthesis of  $CeO_2-ZrO_2$  mixed oxides.

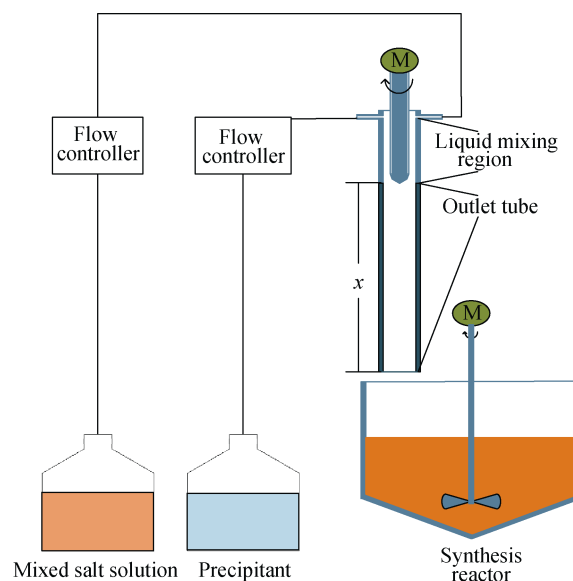


Fig. 1 Schematic diagram for the modified co-precipitation method

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The synthesis reactor consisted of a liquid mixing region and an outlet tube on the upper and a slurry collector under the outlet tube. When the mixed salt solution and the precipitant were pumped into the liquid mixing region, the two fluids were mixed together with stirring and the crystal nucleus would start to form. Then the mixed fluids with crystal nucleus flowed down along the inner wall of the outlet tube and were collected by the slurry collector. Meanwhile, the grains initiated to grow. When the length of the outlet tube increased, the time for grains to grow up would become longer.

## 1.2 Synthesis of CeO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides

CeO<sub>2</sub>-ZrO<sub>2</sub> materials with Ce/Zr molar ratio of 3/2 were prepared by the modified co-precipitation method. Firstly, Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O and ZrO(CO<sub>3</sub>) precursors were dissolved in distilled water and nitric acid solution, respectively, and then mixed. Finally, the precipitates were obtained by dropping ammonia. During this process, the length of the outlet tube was adjusted to 0, 20, 40 and 80 cm, respectively, to gradually extend the time for grains growing. Afterwards, the obtained precipitates were filtered and dried at 120°C for 12 h. The dried precipitate powders were marked as CZ-*x*-d (*x* = 0, 20, 40 and 80). A portion of the precipitate powders were calcined at 600°C for 3 h in air to obtain the fresh samples, which were labeled as CZ-*x*-f, and the aged samples were obtained by thermal treating at 1000°C in air for 5 h, which were assigned as CZ-*x*-a.

## 1.3 Preparation of three-way catalysts (TWCs)

Further considering the applications of the obtained CZ-80 in TWCs, the corresponding Pd/CZ-*x* (*x* = 0, 80) catalysts with 1.5wt% Pd were prepared by impregnation method to study the effects of the modified co-precipitation method. The coating amount onto honeycomb cordierites (Corning, USA, 400 cells/inch<sup>2</sup>, 2.5 cm<sup>3</sup>) was 160 g/L. The obtained samples were calcined at 600°C in air for 3 h to obtain the fresh catalysts, which were marked as Pd/CZ-*x*-f. The aged catalysts were gained by aging at 1000°C in air for 5 h, which were labeled as Pd/CZ-*x*-a.

## 1.4 Evaluation of catalytic performance

The catalytic performance of TWCs was evaluated in a multiple fixed-bed continuum flow micro-reactor with the inlet gas mixture simulated as the automobile exhaust gases, including CO (0.6%), C<sub>3</sub>H<sub>8</sub> (0.06%), NO (0.06%), CO<sub>2</sub> (12%), H<sub>2</sub>O (10%), O<sub>2</sub> (adjustable) and the balance gas N<sub>2</sub>. The gas space velocity was 40,000 h<sup>-1</sup>. The concentrations of the effluent C<sub>3</sub>H<sub>8</sub>, CO, and NO were analyzed by a FGA-4100 five-component analyzer (Foshan

Analysis Instrument Co., Ltd., China). The excess air ratio ( $\lambda$ ) is defined as  $\lambda = \{2[\text{O}_2] + [\text{NO}]\} / \{10[\text{C}_3\text{H}_8] + [\text{CO}]\}$ , and controlled at  $\lambda = 1$  during the catalytic activity measurements.

## 1.5 Characterization

The X-ray diffraction (XRD) patterns of all samples were determined by a Rigaku DX-2500 diffractometer equipped with Cu K $\alpha$  ( $\lambda = 0.15406$  nm). The X-ray tube was operated at 40 kV and 30 mA. All samples were scanned with a step of 0.06° in the range of  $20^\circ \leq 2\theta \leq 70^\circ$ .

The textural properties of the ceria-zirconia mixed oxides were analyzed by N<sub>2</sub> adsorption/desorption at 77 K by the Quantachrome S-30 surface area and pore size analyzer. The specific surface area and the pore size distribution were calculated by the Brunauer-Emmett-Teller (BET) and Barret-Joyner-Halenda (BJH) methods, respectively.

Transmission electron microscopy (TEM) images of the samples were taken using a Tecnai G<sup>2</sup> F20 S-TWIN TEM (FEI Company, USA, 200 kV accelerating voltage). The mean particle sizes of the CeO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides were calculated from TEM images by averaging 30 points of the oxide particles.

# 2 Results and discussions

## 2.1 X-ray diffraction analysis (XRD)

The XRD patterns of all the samples are displayed in Fig. 2. The average crystallite sizes and the lattice parameters are also exhibited in Table 1. Firstly, all the precipitates exhibit the characteristic peaks of cubic fluorite-like CeO<sub>2</sub> phase. This suggests that only few Zr atoms have inserted into the CeO<sub>2</sub> lattice. In the ceria-zirconia system, insertion of Zr<sup>4+</sup> with smaller ionic radius (0.084 nm) compared to the 8-coordinated Ce<sup>4+</sup> ion (0.097 nm) into the CeO<sub>2</sub> lattice could decrease the cell volume and create more structural defects<sup>[13-15]</sup>. Thus, smaller lattice constant indicates that more Zr atoms have inserted into the CeO<sub>2</sub> lattice. The lattice constants of CZ-0-d, CZ-20-d, CZ-40-d and CZ-80-d were calculated to be 0.5421, 0.5422, 0.5380 and 0.5380 nm, respectively. This suggests that much more Zr atoms have inserted into the lattice of CZ-40-d and CZ-80-d. Moreover, the grain size of the samples follows a decreasing tendency of CZ-80-d > CZ-40-d > CZ-20-d > CZ-0-d. It is obvious that the primary grain size increases with the length of the outlet tube. Therefore, a conclusion can be drawn that longer outlet tube contributes to the growth of crystallites in the initial precipitate particles.

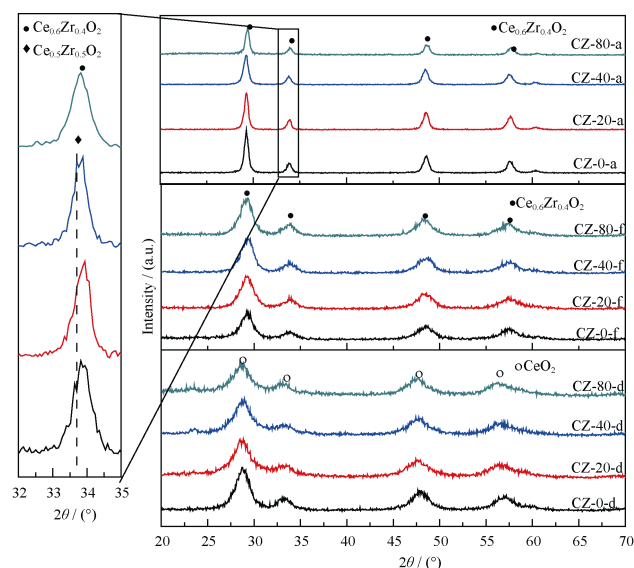


Fig. 2 XRD patterns of the precipitates, fresh samples and aged samples

**Table 1** The crystalline phases, lattice parameters and crystallite sizes of the precipitates, fresh samples and aged samples

Samples	Phase composition	Lattice parameter/nm	Crystallite size/nm
CZ-0-d	Cubic	0.5421	3.7
CZ-20-d	Cubic	0.5422	3.8
CZ-40-d	Cubic	0.5380	4.0
CZ-80-d	Cubic	0.5380	4.3
CZ-0-f	Cubic	0.5274	4.8
CZ-20-f	Cubic	0.5284	4.8
CZ-40-f	Cubic	0.5271	5.0
CZ-80-f	Cubic	0.5291	4.9
CZ-0-a	Cubic + tetragonal	0.5258 <sup>a</sup>	21.2
CZ-20-a	Cubic + tetragonal	0.5261 <sup>a</sup>	19.3
CZ-40-a	Cubic + tetragonal	0.5286 <sup>a</sup>	17.2
CZ-80-a	Cubic	0.5292	14.5

<sup>a</sup> Crystallite size based on the cubic phase.

After thermal treatment at 600°C for 3 h, all the diffraction peaks become narrower and sharper and all the  $2\theta$  values shift to higher angles. This indicates that much more Zr atoms have inserted into the CeO<sub>2</sub> lattice to form solid solutions, and the symmetrical peaks indicate that all the fresh samples are single-phase solid solutions, which is characteristic of cubic Ce<sub>0.6</sub>Zr<sub>0.4</sub>O<sub>2</sub> phase<sup>[12]</sup>. After aging at 1000°C for 5 h, all the diffraction peaks become even narrower and sharper (Fig. 2), indicating that all the aged samples undergo a rapid crystallite growth process (Table 1)<sup>[16]</sup>. Apparent peak splitting is observed in CZ-0-a, CZ-20-a and CZ-40-a, which indicates that phase segregation has occurred in these samples. However, no peak splitting is observed in CZ-80-a which still maintains the single cubic Ce<sub>0.6</sub>Zr<sub>0.4</sub>O<sub>2</sub> phase, suggesting that CZ-80 own superior structural

property. Generally, single-phase CeO<sub>2</sub>-ZrO<sub>2</sub> solid solutions usually own better textural property, thermal stability and redox behaviors with respect to phase-segregated nonhomogeneous ones<sup>[3,17]</sup>. Except for the phase variation, the grain sizes of CZ-0-a, CZ-20-a, CZ-40-a and CZ-80-a have increased greatly, which are 21.2, 19.3, 17.2 and 14.5 nm, respectively. For fine particles, due to the rapid grain growth during thermal aging, pores are agglomerated by moving the grain boundaries<sup>[18]</sup>. The grain size of CZ-80-a is apparently smaller than those of others, which indicates that material CZ-80 is more stable than others. However, from the point of view of grain sintering, material CZ-80 owns the biggest primary grain size (4.3 nm) which turns out to be the smallest (14.5 nm) after thermal aging at 1000°C. For comparison, material CZ-0 has the smallest primary grain size (3.7 nm) which is biggest after thermal aging (21.2 nm). This suggests that less primary grains have sintered together during the high temperature aging, and material CZ-80 exhibits superior structural property and thermal stability.

## 2.2 Textural characterization

The textural properties of the samples were characterized by BET method. The results, including specific surface areas, pore volumes and average pore radii, are summarized in Table 2. As shown in Table 2, the surface areas and pore volumes of the fresh samples are all above 110 m<sup>2</sup>/g and 0.25 cm<sup>3</sup>/g, respectively, indicating that all fresh samples own good textural property. After calcined at 1000°C for 5 h, the specific surface areas of all the samples obviously reduce by severe aggregation of the nano-particles, and their accumulative pore volumes also remarkably decrease. Compared with other samples, however, CZ-80-a maintains higher surface area of 29 m<sup>2</sup>/g and larger pore volume of 0.13 cm<sup>3</sup>/g which are 13 m<sup>2</sup>/g and 0.05 cm<sup>3</sup>/g higher than those of CZ-0-a, respectively. These results indicate that CZ-80 has the best textural property with good thermal stability.

In order to study the pore structure and sintering

**Table 2** Textural properties of fresh and aged samples

Samples	Specific surface/(m <sup>2</sup> ·g <sup>-1</sup> )	Pore volume/(cm <sup>3</sup> ·g <sup>-1</sup> )	Average pore radius/nm
CZ-0-f	118	0.25	4.2
CZ-20-f	137	0.27	3.9
CZ-40-f	120	0.27	4.5
CZ-80-f	129	0.30	4.6
CZ-0-a	16	0.08	10.7
CZ-20-a	15	0.07	9.3
CZ-40-a	22	0.11	10.2
CZ-80-a	29	0.13	9.0

behavior of the samples, the corresponding BJH pore size distribution curves of the fresh and aged samples are depicted in Fig. 3 and Fig. 4. For the fresh samples, the detailed statistical data (Table 3) calculated from Fig. 3 show great differences among these samples. Firstly, the proportions of the pores distributed below 3 nm decrease in the order of CZ-0-f  $\approx$  CZ-20-f > CZ-40-f > CZ-80-f. The proportions of the pores distributed between 3–6 nm for CZ-0-f, CZ-20-f, CZ-40-f and CZ-80-f are 32.7%, 31.1%, 40.6% and 47.8%, respectively. And the proportions of the pores distributed above 6 nm for all the fresh samples are almost the same. After aging at 1000°C for 5 h, the pore size distributions of the samples have changed drastically (Fig. 4 and Table 4). From the statistical data listed in Table 4, the proportions of the pores distributed between 6–16 nm for CZ-0-a, CZ-20-a, CZ-40-a and CZ-80-a are 43.7%, 49.6%, 63.0% and 77.5%, respectively. For CZ-80-a, the proportions of the pores distributed below 6 nm and above 16 nm are both very small. This indicates that the pore size distribution of CZ-80-a is more concentrated than those of others. Combined with its bigger pore volume, this indicates that the pore structure of CZ-80 is more stable than those of others, and this result could also account for its superior textural property. Furthermore, the above proportions of the pores distributed between 3–6 nm

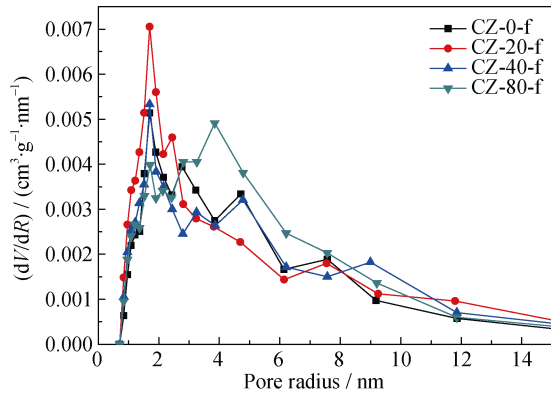


Fig. 3 Pore size distributions of fresh samples

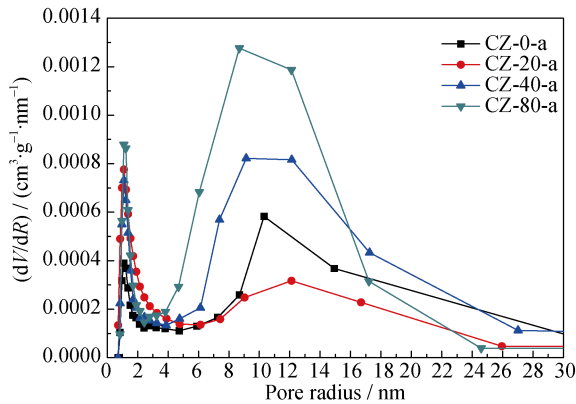


Fig. 4 Pore size distribution of aged samples

Table 3 Statistical data of the proportion of pore radius for pore size distribution of fresh samples

Samples	Below 3 nm	Between 3 nm and 6 nm	Above 6 nm
CZ-0-f	37.6%	32.7%	29.7%
CZ-20-f	39.0%	31.1%	29.9%
CZ-40-f	30.1%	40.6%	29.3%
CZ-80-f	22.8%	47.8%	29.4%

Table 4 Statistical data of the proportion of pore radius for pore size distribution of aged samples

Samples	Below 6 nm	Between 6 nm and 16 nm	Above 16 nm
CZ-0-a	10.0%	43.7%	46.3%
CZ-20-a	26.3%	49.6%	24.1%
CZ-40-a	14.3%	63.0%	22.7%
CZ-80-a	12.9%	77.5%	9.6%

in fresh samples might be related to the different sintering behavior of the pore structure in different samples. These results make us speculate that the bigger average pore radius with higher percentage of large pores is key parameter for the materials with high thermal stability.

2.3 Transmission electron microscopy (TEM)

The morphologies of CZ-0 and CZ-80 were investigated by TEM, and the results are shown in Fig. 5. The average grain sizes of CZ-0 and CZ-80 are calculated with the help of Digital Micrograph, and the results are shown in Table 5. From Fig. 5, it can be observed that both precipitates are composed of many sphere-like nanoclusters with similar packing modes. The average grain sizes of CZ-80-d and CZ-0-d are 4.3 nm and 3.3 nm, respectively.

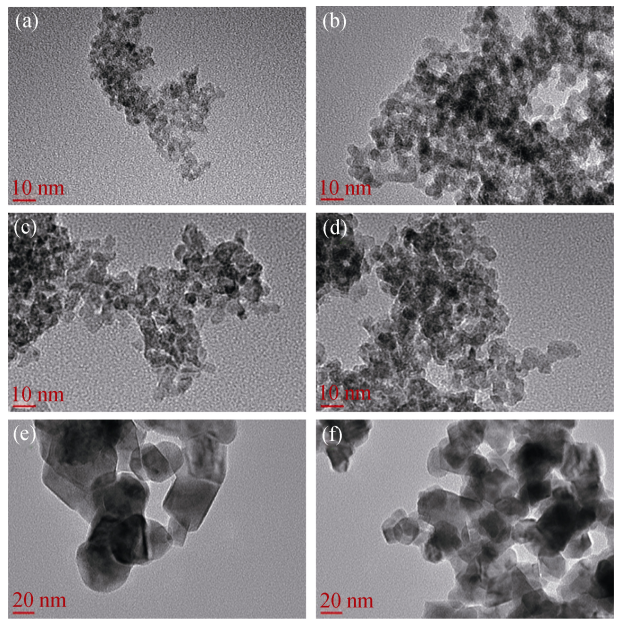


Fig. 5 TEM images of samples (a) CZ-0-d; (b) CZ-80-d; (c) CZ-0-f; (d) CZ-80-f; (e) CZ-0-a; (f) CZ-80-a



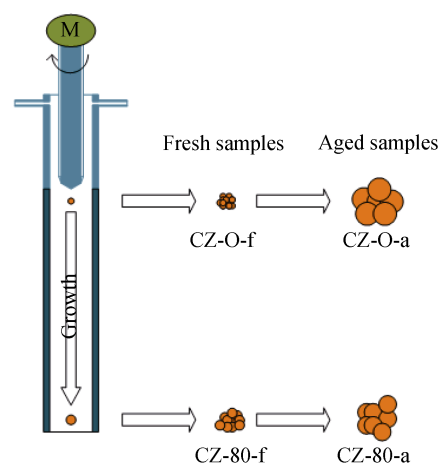
**Table 5** The average grain sizes of CZ-0 and CZ-80 calculated from TEM results

Samples	Precipitates/nm	Fresh samples/nm	Aged samples/nm
CZ-0	3.3	4.8	25.6
CZ-80	4.3	5.1	16.3

The significantly larger grain size of CZ-80-d is quite in accordance with the above XRD results and confirms that the grain size increases with the length of the outlet tube. After thermal treatment at 600°C, the difference of the grain size between CZ-80-f and CZ-0-f declines, but the grain size of CZ-80-f is still larger than that of CZ-0-f. After aging at 1000°C, the average grain sizes of CZ-80-d and CZ-0-d increase to 16.3 nm and 25.6 nm, respectively. From the point of view of sintering, the great divergence in the growth of the grain size from the initial precipitate particles to the 1000°C thermal aged ones in these two samples might be related to the length of the outlet tube. A possible mechanism of grain growth from initial precipitate particles can be proposed as Fig. 6. Contacting with the textural properties and XRD results, it can be speculated that the excellent anti-sintering performance of CZ-80 is attributed to the formation of larger grains at the primary stage of precipitation, and the generation of bigger pores through accumulation of the grains, which are helpful for improving the thermal ability. This might be attributed to that there is more time for the grains to grow up at the primary stage of precipitation when the length of the outlet tube increases to 80 cm. So it can be concluded that the bigger the initial grain size is, the better the thermal stability is.

## 2.4 Catalytic performance

The results of the catalytic activity evaluation performed over the fresh and aged catalysts are summarized in Table 6. For the fresh catalysts Pd/CZ-0-f and Pd/CZ-80-f, the complete transformation temperatures ( $T_{90}$ ) of  $C_3H_8$ , NO and CO are almost the same. This would be attributed to their high surface areas which have provided enough spaces for the dispersion of the metal particles. After aging, both catalysts are deactivated to a certain extent. The  $T_{90}$  of  $C_3H_8$ , NO and CO for Pd/CZ-80-a are 400°C, 290°C and 272°C, respectively,

**Fig. 6** Schematic diagram of growing and sintering process of grains

while the values for Pd/CZ-0-a are 420°C, 298°C and 293°C, respectively. For Pd/CZ-80-a, the  $T_{90}$  of  $C_3H_8$ , NO and CO are 20°C, 8°C and 21°C lower than those of Pd/CZ-0-a. As reported in the previous studies<sup>[3,19]</sup>, the sintering of the support would result in the encapsulation of metal particles and further cause the deactivation of the catalyst. Therefore, the better catalytic performance observed for Pd/CZ-80-a is due to the superior structural property and excellent thermal stability of corresponding support material CZ-80.

## 3 Conclusions

In this study, a series of ceria-zirconia mixed oxides were prepared by a modified co-precipitation method with the synthesis reactor equipped with an outlet tube with different lengths. Based on the results and discussion presented above, the following conclusions can be drawn:

- 1) The primary grain size increases with the length of the outlet tube.
- 2) Sample CZ-80 exhibits superior structural property and thermal stability.
- 3) Sample CZ-80 has the best textural property with good thermal stability. After aging at 1000°C for 5 h in air, the specific surface area and pore volume of CZ-80 are maintained at 29 m<sup>2</sup>/g and 0.13 cm<sup>3</sup>/g, respectively.

**Table 6** Light-off temperatures ( $T_{50}$ ) and complete conversion temperatures ( $T_{90}$ ) for  $C_3H_8$ , NO and CO over fresh and aged catalysts.

Catalysts	$T_{50}/^{\circ}\text{C}$			$T_{90}/^{\circ}\text{C}$		
	$C_3H_8$	NO	CO	$C_3H_8$	NO	CO
Pd/CZ-0-f	273	180	163	325	230	219
Pd/CZ-0-a	358	266	249	420	298	293
Pd/CZ-80-f	270	180	167	326	228	228
Pd/CZ-80-a	332	258	241	400	290	272

4) Higher thermal stability of the catalytic performance of Pd/CZ-80 is also obtained. This has further confirmed that CZ-80 has better prospect in application.

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## 改进共沉淀法以提高三效催化剂中铈锆复合氧化物的热稳定性

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**摘 要:** 采用共沉淀法制备了铈锆材料(铈锆比为 3/2)。通过改进反应器装置(图 1), 延长了初始晶粒生长的时间, 提高了铈锆材料的热稳定性。采用 X 射线衍射(XRD)、氮气吸脱附和透射电镜(TEM)对制备的材料进行了表征。结果表明, 延长初始晶粒生长的时间可以得到较大尺寸的晶粒, 这有利于提高材料的织构和结构性能, 从而提高热稳定性。本研究将该材料应用于单 Pd 三效催化剂, 表现出了优异的活性和热稳定性, 具有良好的应用前景。

**关 键 词:** 铈锆材料; 初始晶粒; 共沉淀法; 热稳定性

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