

Microwave Dielectric Properties of the $(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ Ceramics

LIU Hao, SHEN Chun-Ying, LU Zheng-Dong, QIU Tai

(College of Materials Science and Engineering, Nanjing University of Technology, Nanjing 210009, China)

Abstract: The microwave dielectric properties of the $(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (MCT-CLT) ceramics were investigated. The system was prepared using a conventional solid-state ceramic route. The objective of the present work is to compensate for the negative temperature coefficient of resonant frequency (τ_f) of $(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3$ (MCT) by the addition of $(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (CLT). The microwave dielectric properties are strongly correlated with the sintering temperature and the composition. Very dense MCT-CLT ceramics were prepared by sintering at 1300°C. When the ceramics were sintered at temperatures above 1300°C, the bulk density decreased and the dielectric properties deteriorated. With the increasing of x , the relative dielectric constant (ϵ_r) of the ceramics increases and the product of quality factor and resonant frequency ($Q \times f$) decreases. For practical application, $0.87(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-0.13(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (87MCT-13CLT) ceramics sintered at 1300°C with a dielectric constant $\epsilon_r=22.4$, a $Q \times f$ value of 35000 GHz and a temperature coefficient of resonance frequency (τ_f) of $-8.7 \times 10^{-6}/^\circ\text{C}$ was proposed in this paper.

Key words: $(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ ceramics; microwave dielectric ceramics; dielectric constant; quality factor; temperature stable resonant frequency

Microwave dielectric ceramics are important materials used in microwave devices such as resonators, filters and oscillators in microwave communication systems^[1]. For a good microwave dielectric ceramics, three dielectric characteristics should be satisfied, which are high dielectric constant (ϵ_r) to reduce the size of devices, high quality factor ($Q \times f$) for achieving prominent frequency selectivity and stability, and a near zero temperature coefficient of resonance frequency (τ_f)^[2] for temperature stability respectively.

MgTiO₃-based ceramics is one of the leading dielectric materials for microwave frequency applications. In the past, CaTiO₃ or SrTiO₃ were incorporated to adjust temperature coefficient of resonance frequency of MgTiO₃-based ceramics^[3-4]. Recently, Lu *et al* reported that through partial replacement of Mg by Co, the $(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3$ (MCT) ceramics with ilmenite-type structure possesses good dielectric characteristics ($\epsilon_r = 18.99$, $Q \times f = 154000$ GHz and $\tau_f = -45.6 \times 10^{-6}/^\circ\text{C}$)^[5]. Moreover, $(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (CLT) was another important microwave dielectric ceramic, which shows a positive τ_f value of $213 \times 10^{-6}/^\circ\text{C}$ associated with a high ϵ_r of 109 and a $Q \times f$ value of 17600 GHz^[6]. This work intends to further improve the dielectric properties of MCT, particu-

larly in terms of the $Q \times f$ and τ_f values, by modifying it sequentially with certain contents of CLT. The correlation between the microstructure and the $Q \times f$ value was also investigated.

1 Experimental

High-purity oxide powders (>99.9%) MgO, TiO₂, Co₂O₃, La₂O₃ and CaCO₃ were used as raw materials. MgO and La₂O₃ was separately heated at 700°C and 900°C for 2h before weighing to remove any hydroxides. The powders were weighed according to the desired stoichiometry of CLT and MCT respectively, and mixed for 6 h with distilled water. Then the two mixed powders were calcined at 1100°C for 3h to produce CLT and MCT respectively, and mixed according to the composition of MCT-CLT and re-milled for 6h. After being dried, the resultant mixed powder were pressed into pellets of $\phi 11\text{mm} \times 5\text{mm}$ in thickness under a pressure of 300MPa, which was followed by sintering at 1250–1400°C for 2h.

The microstructures of the sintered samples were observed by scanning electron microscope (SEM) and energy dispersive spectroscope (EDS). X-ray power diffrac-

tion (XRD) data were collected for phase identification using $\text{CuK}\alpha$ radiation. The densities of the samples were measured by the Archimedes method. The dielectric properties of the samples at microwave frequency were measured by the modified Hakki and Coleman's method in the TE011 mode using a network analyzer^[7-8]. τ_f was evaluated in the temperature range from 25°C to 80°C.

2 Results and discussion

2.1 Sintering properties

Figure 1 shows the bulk density of MCT-CLT ceramics sintered at different temperatures. With the increase of sintering temperature, the porosity decreased to a minimal at 1300°C and thereafter slightly increased. Dense ceramics can be obtained when sintered at 1300°C. The decrease of density at 1400°C as compared with 1300°C was owing to the increase of pore size^[9]. The increase of pore size at 1400°C is well visible from the Fig. 3(d). Bulk density was also influenced by the composition and increased with the increase of CLT content, which possesses a higher density than MCT^[10].

2.2 Phase composition

The XRD patterns of MCT-CLT ceramics system did not significantly change with x value ranging from 0.11 to 0.19 sintered at 1300°C for 2 h, as shown in Fig. 2. CLT

has perovskite structure. CLT also has a high ϵ_r of around 109, a $Q \times f$ value higher than 17600 GHz and a large τ_f value of $212 \times 10^{-6}/^\circ\text{C}$. According to the well-known mixing rules, the addition of CLT to the MCT system can enhance the dielectric constant and adjust the temperature coefficient of dielectric constant to near zero. When CLT was added to MCT to form a ceramic system of MCT-CLT, the lattice parameters of MCT did not change with CLT content. Furthermore, the formation of mixed phases in the MCT-CLT ceramics system was due to structural differences and because the average ionic radii of Ca^{2+} (0.099 nm) and La^{3+} (0.115 nm) were larger than those of Mg^{2+} (0.066 nm) and Co^{2+} (0.0745 nm).

2.3 Microstructure

The SEM micrographs of 0.87MCT-0.13CLT ceramics sintered at different temperatures are illustrated in Fig. 3. The grain size of the materials slightly increased with increasing sintering temperature and very dense materials with uniform grain size and morphology was obtained. However, inhomogeneous grain growth was observed at the sintering temperatures higher than 1350°C, indicating 1300°C should be an appropriate sintering temperature for the ceramics. The EDS patterns of 0.87MCT-0.13CLT ceramics sintered at 1300°C are shown in Fig. 4. EDS analysis of Fig. 3(b) indicated that the grain A and B were MCT and CLT respectively, which further verified the MCT-CLT system.

2.4 Microwave dielectric properties

Figure 5 demonstrates the dielectric constant of the MCT-CLT ceramics sintered at different temperatures. Variation of the ϵ_r value was consistent with that of density and the maximum dielectric constant was obtained for each composition when sintered at 1300°C. As can be expected from mixing rule, the dielectric constant increased from 21.86 to 26.65 as the content of CLT increased from 0.11 to 0.19, owing to a much higher ϵ_r value of CLT than MCT. It also suggests an ϵ_r -tunable system through the control of the x value. The quality factor value ($Q \times f$) of

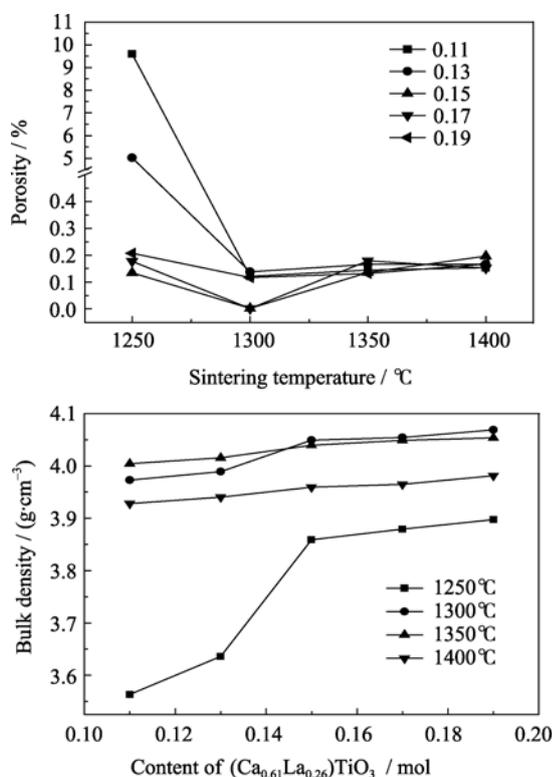


Fig. 1 Bulk density and Porosity of MCT-CLT ceramics system sintered at different temperatures

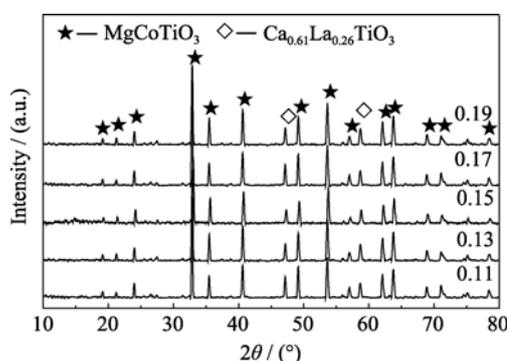


Fig. 2 XRD patterns of MCT-CLT ceramics sintered at 1300°C for 2 h

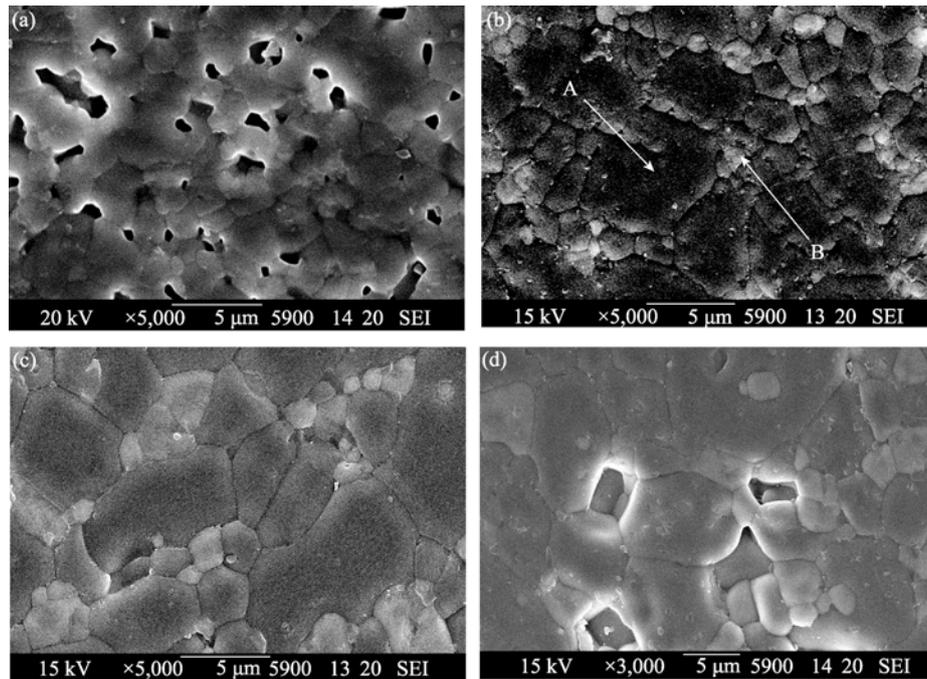


Fig. 3 SEM images of 0.87MCT-0.13CLT ceramics sintered at different temperatures (a) 1250 °C; (b) 1300 °C; (c) 1350 °C; (d) 1400 °C

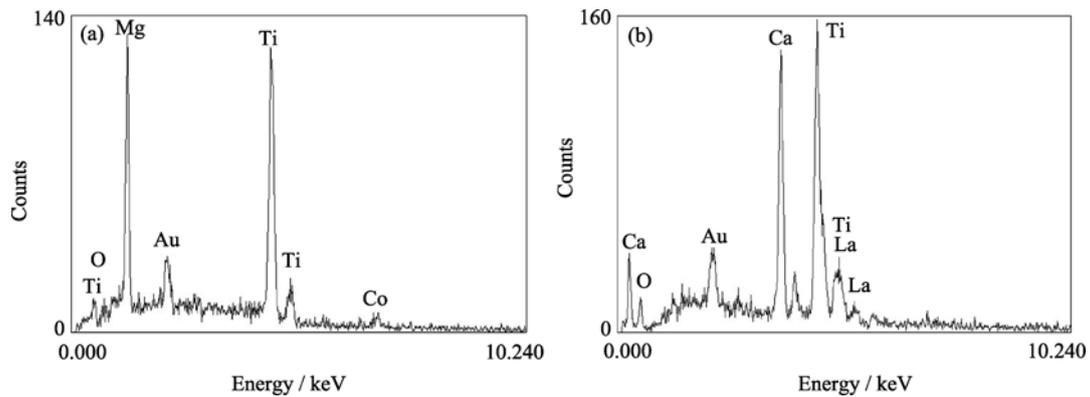


Fig. 4 EDS patterns of 0.87MCT-0.13CLT ceramics in Fig.3 (b) (a) A spot; (b) B spot

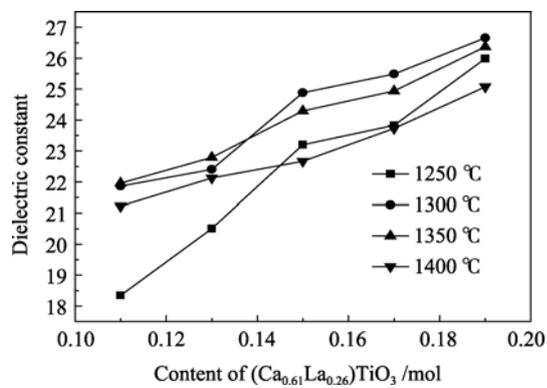


Fig. 5 ϵ_r value of MCT-CLT ceramics system sintered at different temperatures

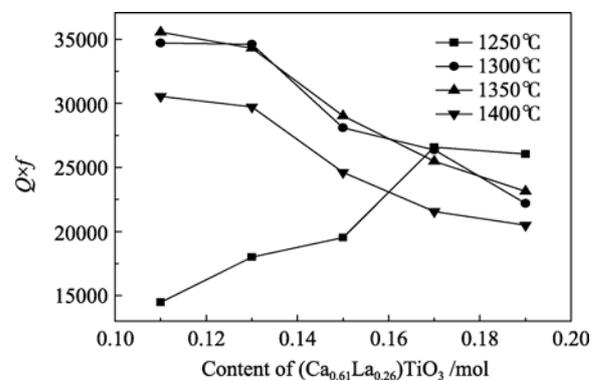


Fig. 6 $Q \times f$ value of MCT-CLT ceramics system sintered at different temperatures

MCT-CLT ceramics sintered at different temperatures are shown in Fig. 6. Many factors are believed to affect the microwave dielectric loss which consists of intrinsic loss and extrinsic loss. Intrinsic losses are mainly caused by lattice vibration modes while extrinsic losses are dominated by the second phases, oxygen vacancies, grain size. Meanwhile, relative density also plays an important role in controlling the dielectric loss, and has been shown for other microwave dielectric materials^[11-12].

Since the quality factor of MCT ($Q \times f = 154000 \text{GHz}$) is much higher than that of CLT ($Q \times f = 17600 \text{GHz}$), a decrease in the $Q \times f$ value is expected as the amount of CLT increased. The $Q \times f$ value of MCT-CLT ceramics decreased with increasing x value in all cases. The 0.87MCT-0.13CLT ceramics possessed an excellent $Q \times f$ value of 35000 GHz at 1300°C for 2h.

Figure 7 illustrates the temperature coefficient of the resonant frequency (τ_f) of MCT-CLT ceramics sintered at 1300°C. In general, τ_f is related to the phase composition of the ceramics and insensitive to the sintering temperature. A higher CLT ($\tau_f = 213 \times 10^{-6}/^\circ\text{C}$) content leads to a variation of τ_f toward positive value, which increases from $-19.4 \times 10^{-6}/^\circ\text{C}$ to $27.8 \times 10^{-6}/^\circ\text{C}$ as the addition of CLT increases from 0.11 to 0.19. It gives a cross-zero line which implies that zero τ_f can be achieved through appropriate adjustment of the x value in the system.

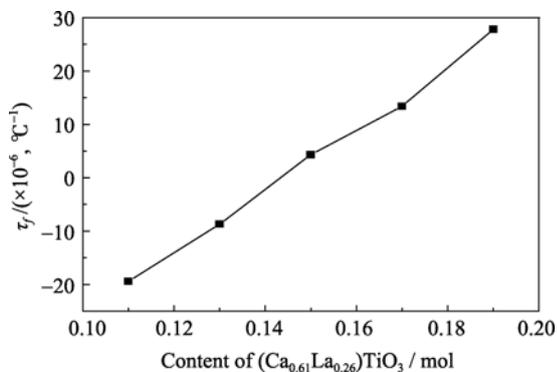


Fig.7 The τ_f value of MCT-CLT ceramics system sintered at different temperatures

3 Conclusions

Very dense MCT-CLT ceramics were prepared by sintering at 1300°C, which exhibited optimum dielectric properties. When the ceramics were sintered at temperatures above 1300°C, the increase of pore size resulted in the decrease in density and degradation in dielectric properties.

With the molar fraction of CLT in MCT-CLT ceramics

increasing from 0.11 to 0.19, both ϵ_r and τ_f value increased, whereas $Q \times f$ value decreased gradually. The ϵ_r , $Q \times f$ and temperature coefficient of resonant frequency (τ_f) of 0.87MCT-0.13CLT ceramic sintered at 1300°C are 22.4, 35000GHz and $-8.7 \times 10^{-6}/^\circ\text{C}$, respectively.

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$(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ 陶瓷的微波介电性能

刘昊, 沈春英, 卢正东, 丘泰

(南京工业大学 材料科学与工程学院, 南京 210009)

摘要: 研究了 $(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (MCT-CLT) 体系陶瓷的微波介电性能. 目的是通过 $(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ (CLT) 协调 $(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3$ (MCT) 陶瓷的谐振频率温度系数. 实验发现, 烧结温度和陶瓷组成对微波介电性能影响显著, 当烧结温度为 1300°C 时, 可以获得良好的致密度, 当烧结温度超过 1300°C 时, 陶瓷致密度和介电性能下降. 此外, 随着 CLT 含量的增加, 材料的介电常数增大, 品质因数减小. 当 CLT 含量为 13%, 烧结温度为 1300°C , 保温 2h, (MCCLT) 陶瓷具有优良微波介电性能, $\epsilon_r=22.4$, $Q \times f=35000$ GHz, $\tau_f=-8.7 \times 10^{-6}/^\circ\text{C}$, 从而达到实用要求.

关键词: $(1-x)(\text{Mg}_{0.9}\text{Co}_{0.1})\text{TiO}_3-x(\text{Ca}_{0.61}\text{La}_{0.26})\text{TiO}_3$ 陶瓷; 微波介质陶瓷; 介电常数; 品质因数; 谐振频率温度系数
中图分类号: TQ174 **文献标识码:** A